

Collective Effects and Instabilities

G. Wang

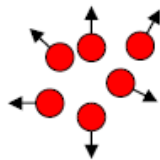
Outline

- Introduction
 - Collective effects, collective instabilities
- Wakefields and Impedances (Ultra-relativistic model)
 - Wake functions
 - Panofsky-Wenzel theorem
 - Cylindrical symmetric structure
 - Wake potentials, loss factor and kick factor
 - Impedances
- Single bunch beam breakup (Two particle model)

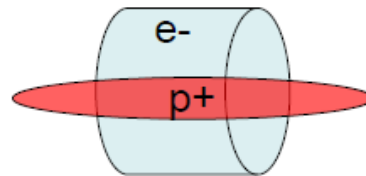
What are collective effects?

- In the single particle dynamics, **the E&M fields** due to the charged particle **themselves** are neglected when considering their motions.
- As the number of the charged increases, the particles' own fields (and fields induced by them) can start to affect its behavior, which is generally called the **collective effects**.

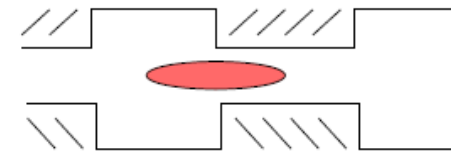
Beam interacts with itself: space charge, IBS, Touschek effects



Beam interacts with localized electron cloud or ion cloud



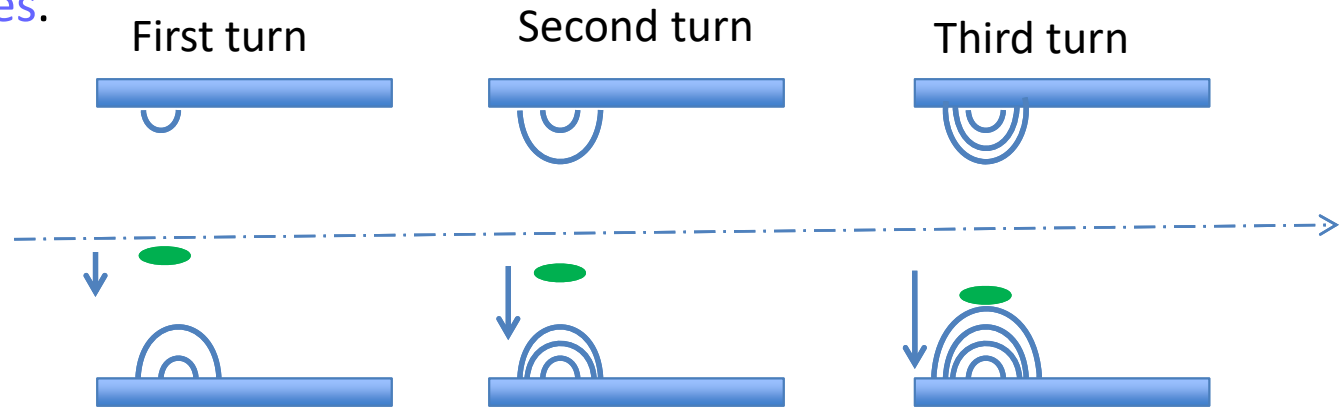
Beam interacts with machine: impedances-related instabilities.



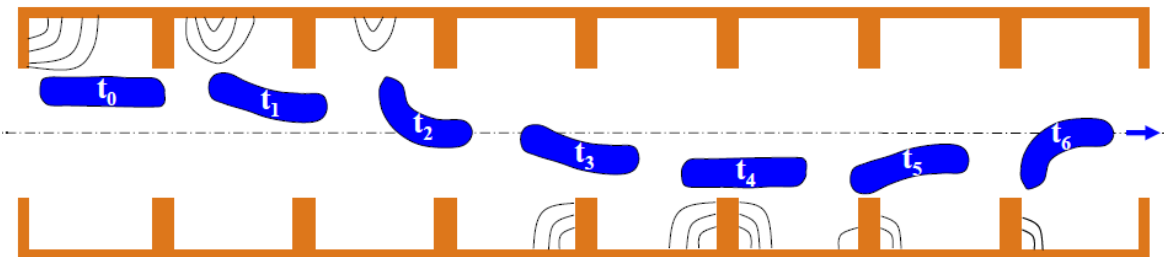
Collective instabilities

- The particle beam interacts with its surroundings to generate an electromagnetic field, known as wakefield. This field then acts back on the beam, perturbing its motion.
- Under unfavorable conditions, the perturbation on the beam are continuously enhanced by the wakefield, leading to the collective instabilities.

Example 1: multi-pass BBU in ERL

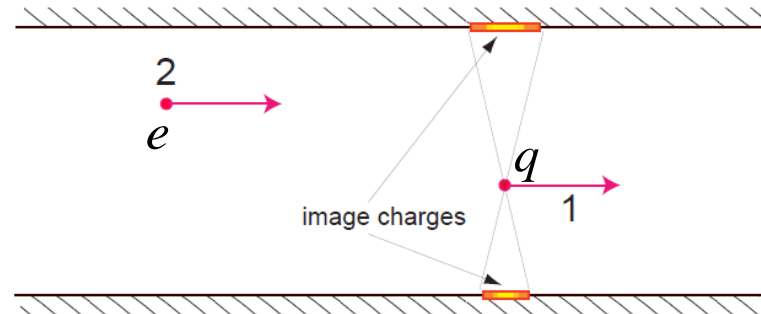
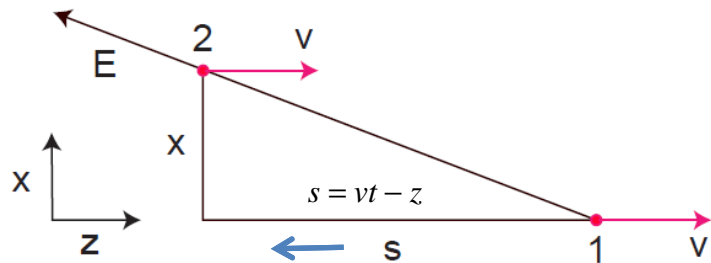


Example 2: single bunch BBU



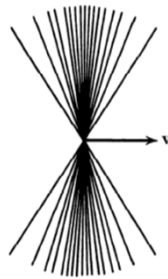
- For the rest of the lecture, we will focus on a wakefield model developed for an ultra-relativistic beam, $\gamma \gg 1$

Ultra-relativistic beam and cylindrical perfect conducting beam pipe



$$\vec{E} = \frac{q\vec{R}}{4\pi\epsilon_0\gamma^2 R^{*3}} \quad \vec{B} = \frac{\vec{\beta}}{c} \times \vec{E}$$

$$R^{*2} = s^2 + x^2 / \gamma^2$$



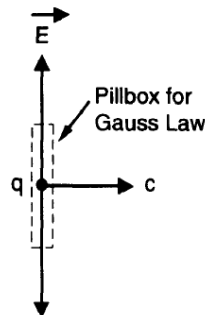
$$F_z = qE_z = -\frac{qes}{4\pi\epsilon_0\gamma^2 (s^2 + x^2 / \gamma^2)^{3/2}}$$

$$F_x = q(E_x - c\beta B_y) = \frac{qex}{4\pi\epsilon_0\gamma^4 (s^2 + x^2 / \gamma^2)^{3/2}}$$

At the limit of $\gamma \rightarrow \infty$ (Homework)

$$\vec{E} = \frac{q\hat{r}}{2\pi\epsilon_0 r} \delta(z - ct)$$

$$\vec{B} = \frac{\hat{z}}{c} \times \vec{E}$$



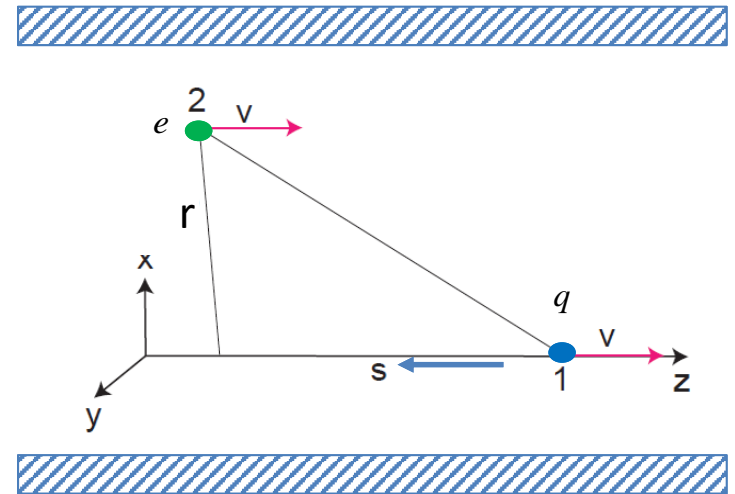
For $\gamma \rightarrow \infty$, interaction among the particles and their images from the wall vanishes if

1. the wall is perfectly conducting, and
 2. there are no discontinuities (cavities, bpms, bellows...).
- (It is also assumed that particles go straight, i.e. no radiations from particles)

Wake Functions

- Rigid bunch approximation:
the motion of particles is not affected while passing through the structure
- Impulse approximation:
instead of the detailed E&M field in the structure, we care more about the total momentum change to the particles due to the wake field:

$$\Delta\vec{p}(x,y,s) = e \int_{-\infty}^{\infty} dt \left[\vec{E}(x,y,z,t) + c\hat{z} \times \vec{B}(x,y,z,t) \right]_{z=ct-s}$$



Longitudinal wake function*: $w_l(x,y,s) = -\frac{c}{qe} \Delta p_z = -\frac{c}{q} \int_{-\infty}^{\infty} E_z(x,y,ct-s,t) dt$ [V/C]

Transverse wake function*: $\vec{w}_t(x,y,s) = \frac{c}{qe} \Delta\vec{p}_\perp = \frac{c}{q} \int_{-\infty}^{\infty} \left[\vec{E}_\perp(x,y,z,t) + c\hat{z} \times \vec{B}(x,y,z,t) \right]_{z=ct-s} dt$ [V/C]

* These definition follow from 'Impedances and Wakes in High-Energy Particle Accelerators' by B. Zotter, which is different from those in 'Physics of Collective Beam Instabilities in High Energy Accelerators' by A. Chao.

Panofsky-Wenzel Theorem

We want to find relation between longitudinal wake function and transverse wake function due to a structure (a piece of beam pipe, bpm, bellow, cavity....)

$$\nabla_s \times \Delta \vec{p}(x, y, s) = \nabla_s \times \int_{-\infty}^{\infty} \vec{F}(x, y, z, t) \Big|_{z=vt-s} dt = \int_{-\infty}^{\infty} [\nabla \times \vec{F}(x, y, z, t)] \Big|_{z=vt-s} dt$$

$$\nabla_s = \hat{x} \frac{\partial}{\partial x} + \hat{y} \frac{\partial}{\partial y} - \hat{z} \frac{\partial}{\partial s}$$

$$\nabla = \hat{x} \frac{\partial}{\partial x} + \hat{y} \frac{\partial}{\partial y} + \hat{z} \frac{\partial}{\partial z}$$

$$\vec{F} = q(\vec{E} + \vec{v} \times \vec{B})$$

$$\nabla \times \vec{F} = q \nabla \times \vec{E} + q \nabla \times (\vec{v} \times \vec{B})$$

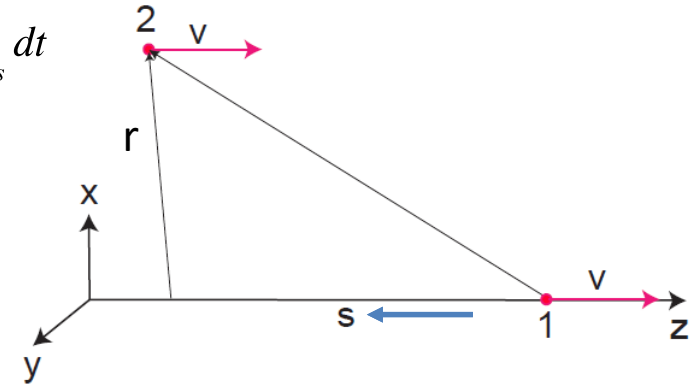
$$= -q \frac{\partial \vec{B}}{\partial t} + q \vec{v} (\nabla \cdot \vec{B}) - q (\vec{v} \cdot \nabla) \vec{B}$$

$$= -q \frac{\partial \vec{B}}{\partial t} - q v \frac{\partial \vec{B}}{\partial z}$$

$$\vec{v} = v \hat{z}$$

$$\nabla \cdot \vec{B} = 0$$

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$



We assume the B field due to the structure has limited spatial range, i.e. it is localized.

$$\nabla_s \times \Delta \vec{p}(x, y, s) = -q \int_{-\infty}^{\infty} \left[\left(\frac{\partial}{\partial t} + v \frac{\partial}{\partial z} \right) \vec{B}(x, y, z, t) \right] \Big|_{z=vt-s} dt = -q \int_{-\infty}^{\infty} \frac{d}{dt} \vec{B}(x, y, vt-s, t) dt = 0$$

$$\frac{\partial}{\partial s} \Delta \vec{p}_\perp = -\vec{\nabla}_\perp \Delta p_z$$

\Rightarrow

$$\frac{\partial}{\partial s} \vec{w}_t(x, y, s) = \vec{\nabla}_\perp w_l(x, y, s)$$

This is called Panofsky-Wenzel theorem

$$[\nabla_\perp \times \Delta \vec{p}_\perp(x, y, s)] \cdot \hat{z} = 0$$

*The derivation follows from USPAS note by K.Y. Ng.

Another Relation at $\beta \rightarrow 1$

$$\nabla_s \cdot \Delta \vec{p}(x, y, s) = \nabla_s \cdot \int_{-\infty}^{\infty} \vec{F}(x, y, z, t) \Big|_{z=vt-s} dt = \int_{-\infty}^{\infty} \left[\nabla \cdot \vec{F}(x, y, z, t) \right]_{z=vt-s} dt$$

$$\begin{aligned} \nabla_s \cdot \Delta \vec{p}(x, y, s) &= -\frac{q}{c} \int_{-\infty}^{\infty} \left[\frac{\partial}{\partial t} E_z(x, y, z, t) \right]_{z=vt-s} dt \\ &= -\frac{q}{c} \int_{-\infty}^{\infty} \left\{ \frac{d}{dt} E_z(x, y, vt-s, t) - \left[v \frac{\partial}{\partial z} E_z(x, y, z, t) \right]_{z=vt-s} \right\} dt \end{aligned}$$

$$\begin{aligned} \nabla \cdot \vec{E} &= \frac{\rho}{\epsilon_0} \quad \vec{j} = \rho v \hat{z} \\ \nabla \times \vec{B} &= \mu_0 \left(\vec{j} + \epsilon_0 \frac{\partial \vec{E}}{\partial t} \right) \end{aligned}$$



$$\begin{aligned} \nabla \cdot \vec{F} &= q \nabla \cdot \vec{E} + q \nabla \cdot (\vec{v} \times \vec{B}) \\ &= q \frac{\rho}{\epsilon_0} - q \vec{v} \cdot (\nabla \times \vec{B}) \\ &= q \frac{\rho}{\epsilon_0} - q \mu_0 \vec{v} \cdot \left(\rho v \hat{z} + \epsilon_0 \frac{\partial \vec{E}}{\partial t} \right) \\ &= q \frac{\rho}{\epsilon_0 \gamma^2} - \frac{q}{c} \beta \frac{\partial}{\partial t} E_z \\ &\approx -\frac{q}{c} \frac{\partial}{\partial t} E_z \end{aligned}$$

$$\begin{aligned} &= \frac{qv}{c} \int_{-\infty}^{\infty} \left[\frac{\partial}{\partial z} E_z(x, y, z, t) \right]_{z=vt-s} dt \\ &= -\frac{qv}{c} \frac{\partial}{\partial s} \int_{-\infty}^{\infty} E_z(x, y, vt-s, t) dt \\ &\approx -\frac{\partial}{\partial s} \Delta p_z(x, y, s) \end{aligned}$$

$$\boxed{\nabla_{\perp} \cdot \Delta \vec{p}(x, y, s) = 0}$$

Cylindrical symmetric structure I

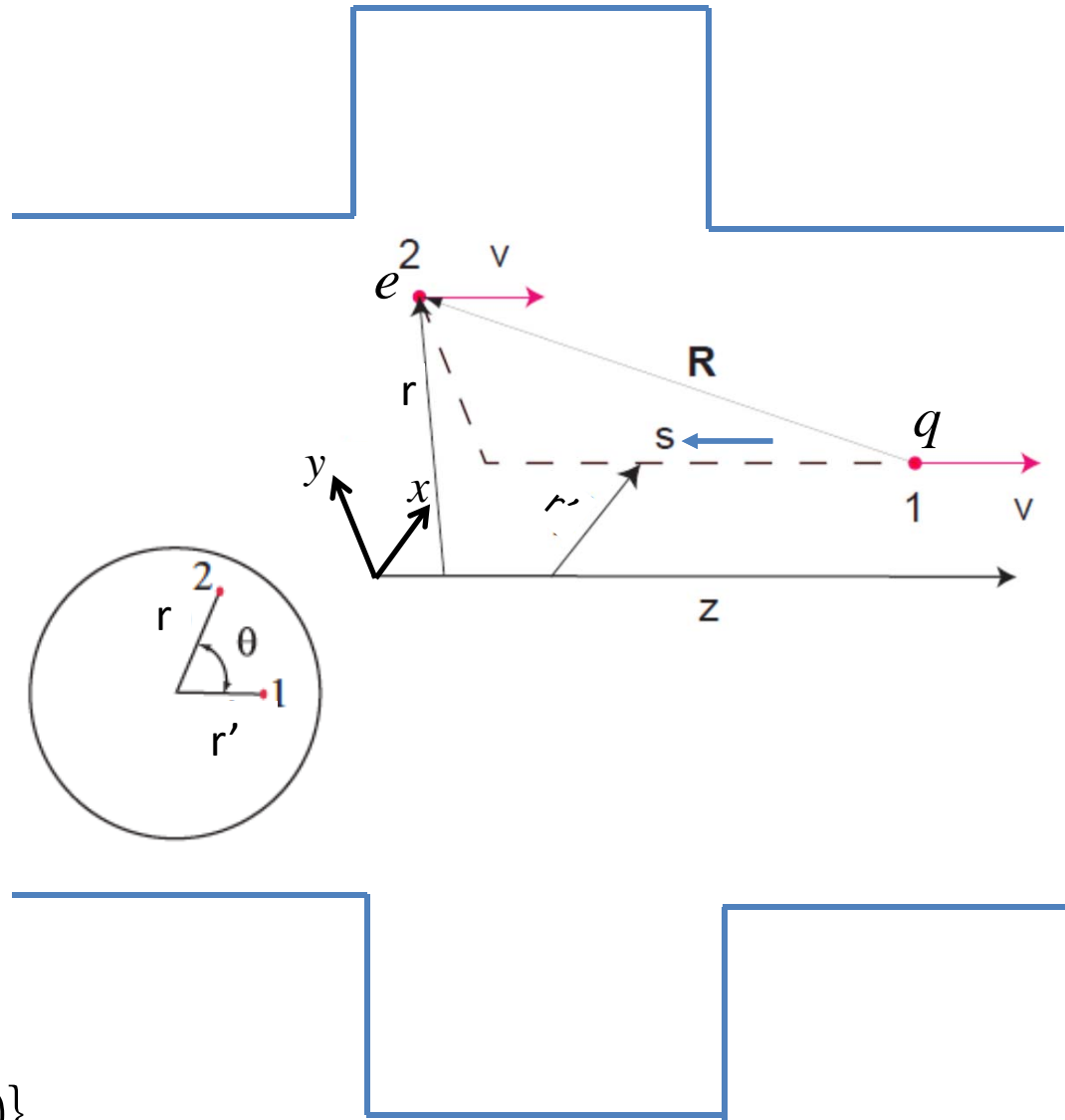
$$\nabla_s \times \Delta \vec{p}(r', r, \theta, z) = 0$$

$$\Rightarrow \begin{cases} \frac{\partial}{\partial s} \Delta \vec{p}_\perp = -\vec{\nabla}_\perp \Delta p_z \\ [\nabla_\perp \times \Delta \vec{p}_\perp] \cdot \hat{z} = 0 \end{cases}$$

$$\nabla_\perp \cdot \Delta \vec{p}(r', r, \theta, s) = 0$$

For a system with cylindrical symmetry, it is usually more convenient to decompose quantities into azimuthal modes:

$$\Delta \vec{p}(r', r, \theta, s) \sim \{ \cos(m\theta), \sin(m\theta) \}$$



Cylindrical symmetric structure II

$$\frac{\partial}{\partial s} \Delta \vec{p}_\perp = -\vec{\nabla}_\perp \Delta p_z \Rightarrow \begin{cases} \frac{\partial}{\partial s} \Delta p_\theta = -\frac{1}{r} \frac{\partial}{\partial \theta} \Delta p_z & \Delta p_r(r', r, \theta, s) = \sum_{m=0}^{\infty} \Delta \tilde{p}_{m,r}(r', r, s) \cos(m\theta) \\ \frac{\partial}{\partial s} \Delta p_r = -\frac{\partial}{\partial r} \Delta p_z & \Rightarrow \Delta p_z(r', r, \theta, s) = \sum_{m=0}^{\infty} \Delta \tilde{p}_{m,z}(r', r, s) \cos(m\theta) \end{cases}$$

$$[\nabla_\perp \times \Delta \vec{p}_\perp(r', r, \theta, s)] \cdot \hat{z} = 0 \Rightarrow \frac{\partial}{\partial r} (r \Delta p_\theta) = \frac{\partial}{\partial \theta} \Delta p_r \Rightarrow \Delta p_\theta(r', r, \theta, s) = \sum_{m=0}^{\infty} \Delta \tilde{p}_{m,\theta}(r', r, s) \sin(m\theta)$$

$$\vec{\nabla}_\perp \cdot \Delta \vec{p}(r', r, \theta, s) = 0 \Rightarrow \frac{\partial}{\partial r} (r \Delta p_r) = -\frac{\partial}{\partial \theta} \Delta p_\theta$$

$$\Rightarrow \begin{cases} \frac{\partial}{\partial s} \Delta \tilde{p}_{m,\theta} = \frac{m}{r} \Delta \tilde{p}_{m,z} & \frac{\partial}{\partial s} \Delta \tilde{p}_{m,r} = -\frac{\partial}{\partial r} \Delta \tilde{p}_{m,z} \\ \frac{\partial}{\partial r} (r \Delta \tilde{p}_{m,\theta}) = -m \Delta \tilde{p}_{m,r} & \frac{\partial}{\partial r} (r \Delta \tilde{p}_{m,r}) = -m \Delta \tilde{p}_{m,\theta} \end{cases} \Rightarrow \frac{\partial}{\partial r} \left[r \frac{\partial}{\partial r} (r \Delta \tilde{p}_{m,r}(r', r, s)) \right] - m^2 \Delta \tilde{p}_{m,r}(r', r, s) = 0$$

$$\Delta \tilde{p}_{m,r}(r, s) = A_m(r', s) m r^{m-1} + \boxed{B_m(r', s) r^{-m-1}}$$

Cylindrical symmetric structure III

By analyzing the source term in the Maxwell equations, it can be shown that the driving term has an explicit dependence on r'

$$\rho = \sum_{m=0}^{\infty} \rho_m \quad \vec{j} = \sum_{m=0}^{\infty} \vec{j}_m, \quad \vec{j}_m = c\rho_m \hat{s},$$

$$\vec{E}, \vec{B} \sim \boxed{I_m = qa^m} \quad A_m(r', s) = \frac{qe}{v} r'^m W_m(s)$$

$$\rho_m = \frac{I_m}{\pi a^{m+1}(1 + \delta_{m0})} \delta(s - ct) \delta(r - a) \cos m\theta,$$

*Reference: A. Chao 'Physics of Collective Beam Instabilities in High Energy Accelerators', eq. (2.35)

$$\Delta \tilde{p}_{m,r}(r, s) = A_m(r', s) m r^{m-1}$$

$$\Delta \tilde{p}_{m,\theta}(r', r, s) = -A_m(r', s) m r^{m-1}$$

$$\Delta \tilde{p}_{m,z} = -A'_m(r', s) r^m$$

Analyzing the
source term in
the Maxwell
equations

$$\Delta \tilde{p}_{m,r}(r, s) = \frac{qe}{v} r'^m W_m(s) m r^{m-1}$$

$$\Delta \tilde{p}_{m,\theta}(r', r, s) = -\frac{qe}{v} r'^m W_m(s) m r^{m-1}$$

$$\Delta \tilde{p}_{m,z}(r', r, s) = -\frac{qe}{v} r'^m W'_m(s) r^m$$

Cylindrical Symmetric Structure IV

$$w_l(r', r, \theta, s) = -\frac{c}{qe} \Delta p_z(r', r, \theta, s) = \sum_{m=0}^{\infty} W'_m(s) r'^m r^m \cos(m\theta)$$

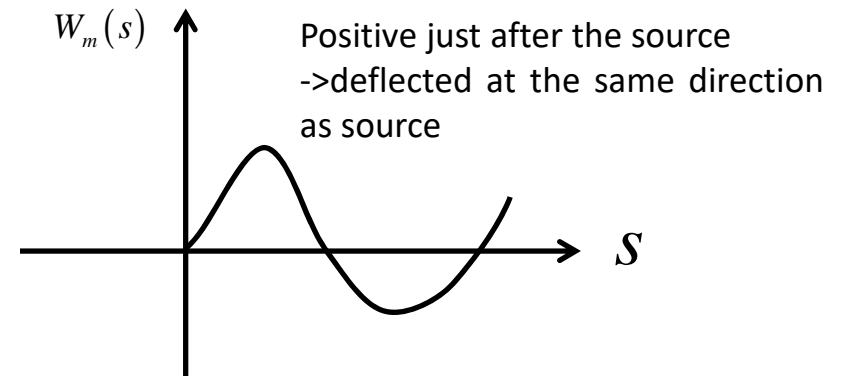
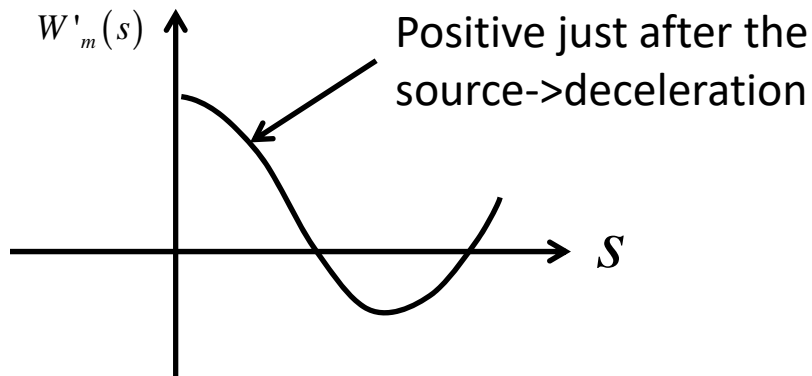
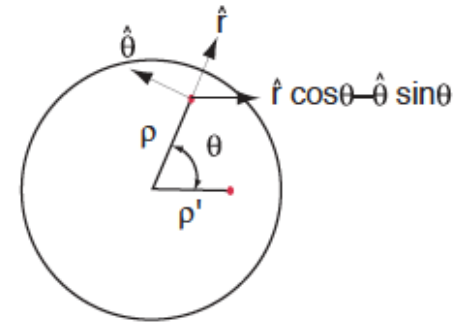
$$\vec{w}_t(r', r, \theta, s) = \frac{c}{qe} \Delta \vec{p}_\perp(r', r, \theta, s) = \sum_{m=0}^{\infty} W_m(s) m r'^m r^{m-1} [\cos(m\theta) \hat{r} - \sin(m\theta) \hat{\theta}]$$

* In many references (by A. Chao, K.Y. Ng ...), $W_m(s)$ and $W'_m(s)$ are called wake functions.

$$m = 0 \quad w_l(r', r, \theta, s) = W'_0(s) \quad w_t(r', r, \theta, s) = 0$$

$$m = 1 \quad \vec{w}_t(r', r, \theta, s) = W_1(s) r' [\cos(\theta) \hat{r} - \sin(\theta) \hat{\theta}]$$

$$w_l(r', r, \theta, s) = W'_1(s) r' r \cos(\theta)$$



Wake Potential

- In practice, usually only monopole mode ($m=0$) wake is considered for longitudinal wake field and only dipole mode ($m=1$) is considered for transverse mode.

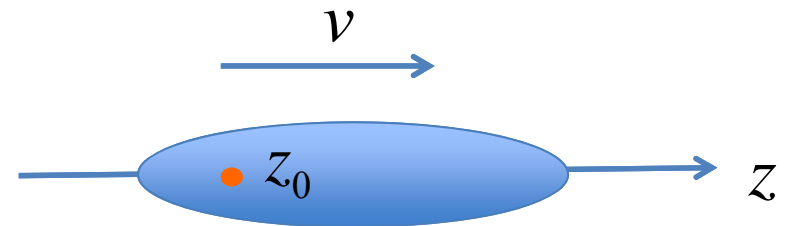
monopole longitudinal wake: $w_{//}(s) = W'_0(s) \quad v/c$

dipole transverse wake: $w_{\perp}(s) = W_1(s) \quad v/(c*m)$

- Wake potentials are defined to describe the momentum change induced by all particles in a bunch to a test unit charge:

$$V_{//}(z_0) = \frac{-c\Delta p_z(z_0)}{eQ_e} = \int_{z_0}^{\infty} \lambda(z_1) w_{//}(z_1 - z_0) dz_1 \quad [V/C]$$

$$\vec{V}_{\perp}(z_0) = \frac{c\Delta \vec{p}_{\perp}(z_0)}{eQ_e} = \int_{z_0}^{\infty} \langle \vec{x}_{\perp}(z_1) \rangle \lambda(z_1) w_{\perp}(z_1 - z_0) dz_1 \quad [V/C]$$



$\lambda(z)$ is line number density of a bunch

* If we observe at $z = z^*$ and use arriving time, $t = \frac{1}{c}(z^* - z)$ as longitudinal variables, above definition become

$$V_{//}(t_0) = \int_{-\infty}^{t_0} \lambda(t_1) w_{//}(t_0 - t_1) dt_1 \quad \vec{V}_{\perp}(t_0) = \int_{-\infty}^{t_0} \langle \vec{x}_{\perp}(t_1) \rangle \lambda(t_1) w_{\perp}(t_0 - t_1) dt_1$$

Loss Factor and Kick Factor

- Once the longitudinal wake potential is known, the total energy change of a bunch to the wakefields is given by

$$\Delta U = - \int_{-\infty}^{\infty} [Q_e V_{//}(z)] [Q_e \lambda(z)] dz$$

Potential at slice (z,z+dz)
Charge in slice (z,z+dz)

Definition of **Loss Factor**:

$$\kappa_{//} \equiv \frac{-\Delta U}{Q_e^2} = \int_{-\infty}^{\infty} V_{//}(z) \lambda(z) dz \quad [\text{V/C}]$$

- Similarly, the total transverse momentum change of a bunch to the wakefields is given by

$$\Delta \vec{P}_{\perp} = \int_{-\infty}^{\infty} \left[e Q_e \frac{\vec{V}_{\perp}(z)}{c} \right] \left[\frac{Q_e}{e} \lambda(z) \right] dz \quad \vec{\kappa}_{\perp} = \frac{c \Delta \vec{P}_{\perp}}{Q_e^2} = \int_{-\infty}^{\infty} V_x(z) \lambda(z) dz \quad [\text{V/C}]$$

Transverse momentum change of a particle at slice (z,z+dz).

Particle number in slice (z,z+dz)

Impedances

- Although the time domain description of particle-environment interaction, the wake fields, contains all informations, it is often more convenient to describe the interaction in frequency domain (convolution vs multiplication, calculate wakes in frequency domain can be easier some times, solving beam instability problems...), i.e. the impedances

$$Z_{//}(\omega) = \frac{1}{c} \int_0^{\infty} w_{//}(s) e^{i\omega s/c} ds \quad [s*V/C]=[Ohm]$$

$$Z_{\perp}(\omega) = -\frac{i}{c} \int_0^{\infty} w_{\perp}(s) e^{i\omega s/c} ds \quad [s*V/(C*m)]=[Ohm/m]$$

- The inverse transformations are

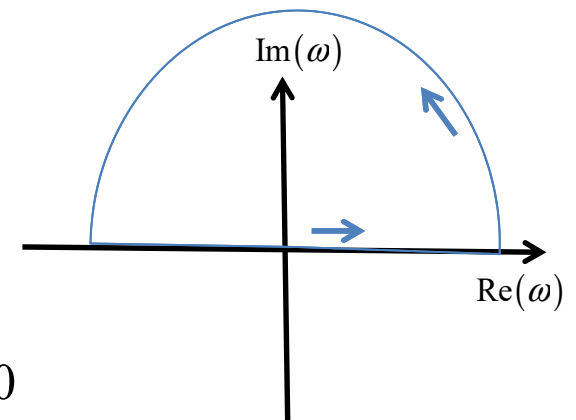
$$w_{//}(s) = \frac{1}{2\pi} \int_{-\infty}^{\infty} Z_{//}(\omega) e^{-i\omega s/c} d\omega$$

$$w_{\perp}(s) = \frac{i}{2\pi} \int_{-\infty}^{\infty} Z_{\perp}(\omega) e^{-i\omega s/c} d\omega$$

* In complex ω plane, $Z_{//}(\omega)$ and $Z_{\perp}(\omega)$ should not have singularities in the upper half plane, i.e. $\text{Im}(\omega) \geq 0$, in order to satisfy the causality condition:

$$w_{//}(s < 0) = 0 \quad w_{\perp}(s < 0) = 0$$

*The frequency ω is frequently allowed to have an imaginary part, in that case the transformation is actually Laplace transform, which is only defined for $\text{Im}(\omega) \geq 0$



Properties of Impedances

- Symmetry properties about positive and negative frequency
(Homework)

$$Z_{//}^*(\omega) = Z_{//}(-\omega) \Rightarrow \begin{cases} \operatorname{Re}[Z_{//}(\omega)] = \operatorname{Re}[Z_{//}(-\omega)] \\ \operatorname{Im}[Z_{//}(\omega)] = -\operatorname{Im}[Z_{//}(-\omega)] \end{cases}$$

$$Z_{\perp}^*(\omega) = -Z_{\perp}(-\omega) \Rightarrow \begin{cases} \operatorname{Re}[Z_{\perp}(\omega)] = -\operatorname{Re}[Z_{\perp}(-\omega)] \\ \operatorname{Im}[Z_{\perp}(\omega)] = \operatorname{Im}[Z_{\perp}(-\omega)] \end{cases}$$

- Relations between real part and imaginary part of impedances

$$w_{//}(s) = \frac{1}{2\pi} \int_{-\infty}^{\infty} Z_{//}(\omega) e^{-i\omega s/c} d\omega \Rightarrow w_{//}(s) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \left\{ \operatorname{Re}[Z_{//}(\omega)] \cos\left(\frac{\omega s}{c}\right) - \operatorname{Im}[Z_{//}(\omega)] \sin\left(\frac{\omega s}{c}\right) \right\} d\omega$$

$$w_{\perp}(s < 0) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \left\{ \operatorname{Re}[Z_{\perp}(\omega)] \cos\left(\frac{\omega s}{c}\right) + \operatorname{Im}[Z_{\perp}(\omega)] \sin\left(\frac{\omega|s|}{c}\right) \right\} d\omega = 0 \Rightarrow \int_{-\infty}^{\infty} \operatorname{Im}[Z_{\perp}(\omega)] \sin\left(\frac{\omega|s|}{c}\right) d\omega = -\int_{-\infty}^{\infty} \operatorname{Re}[Z_{\perp}(\omega)] \cos\left(\frac{\omega|s|}{c}\right) d\omega$$

$$\Rightarrow w_{\perp}(s > 0) = \frac{2}{\pi} \int_0^{\infty} \operatorname{Re}[Z_{\perp}(\omega)] \cos\left(\frac{\omega s}{c}\right) d\omega \quad w_{//}(s > 0) = \frac{2}{\pi} \int_0^{\infty} \operatorname{Im}[Z_{//}(\omega)] \sin\left(\frac{\omega s}{c}\right) d\omega$$

Kramers-Kronig relations:

$$Z_{//}(\omega) = -\frac{i}{\pi} P.V. \int_{-\infty}^{\infty} \frac{Z_{//}(\omega')}{\omega' - \omega} d\omega' \Rightarrow \operatorname{Re}[Z_{//}(\omega)] = \frac{1}{\pi} P.V. \int_{-\infty}^{\infty} \frac{\operatorname{Im}[Z_{//}(\omega')]}{\omega' - \omega} d\omega' \quad \operatorname{Im}[Z_{//}(\omega)] = -\frac{1}{\pi} P.V. \int_{-\infty}^{\infty} \frac{\operatorname{Re}[Z_{//}(\omega')]}{\omega' - \omega} d\omega'$$

Single pass BBU (Two particle model)

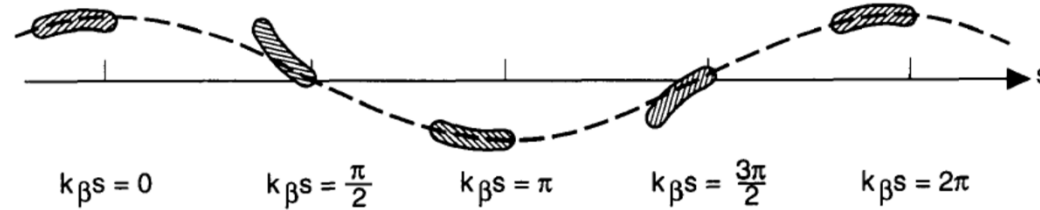
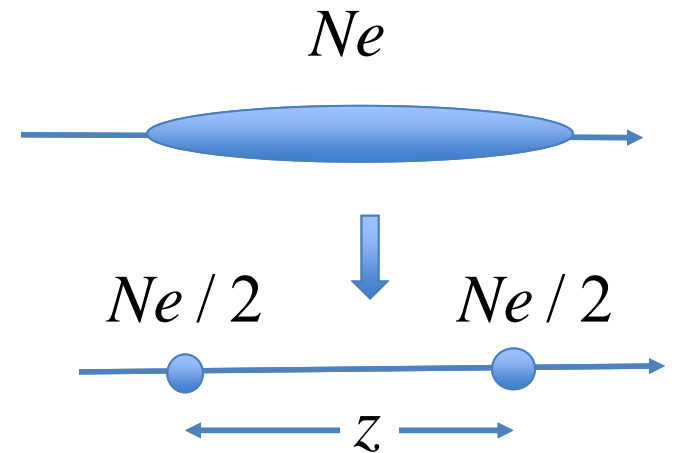


Figure 3.3. Sequence of snapshots of a beam undergoing dipole beam breakup instability in a linac. Values of $k_{\beta}s$ indicated are modulo 2π . The dashed curves indicate the trajectory of the bunch head.

Leading particles $y_1(s) = \hat{y} \cos k_{\beta}s,$

Trailing particles
$$y_2'' + k_{\beta}^2 y_2 = -\frac{Ne^2 W_1(z)}{2EL} y_1$$

$$= -\frac{Nr_0 W_1(z)}{2\gamma L} \hat{y} \cos k_{\beta}s$$



$$y_2(s) = \hat{y} \left[\cos k_{\beta}s - \frac{Nr_0 W_1(z)}{4k_{\beta}\gamma L} s \sin k_{\beta}s \right],$$

Single pass BBU II

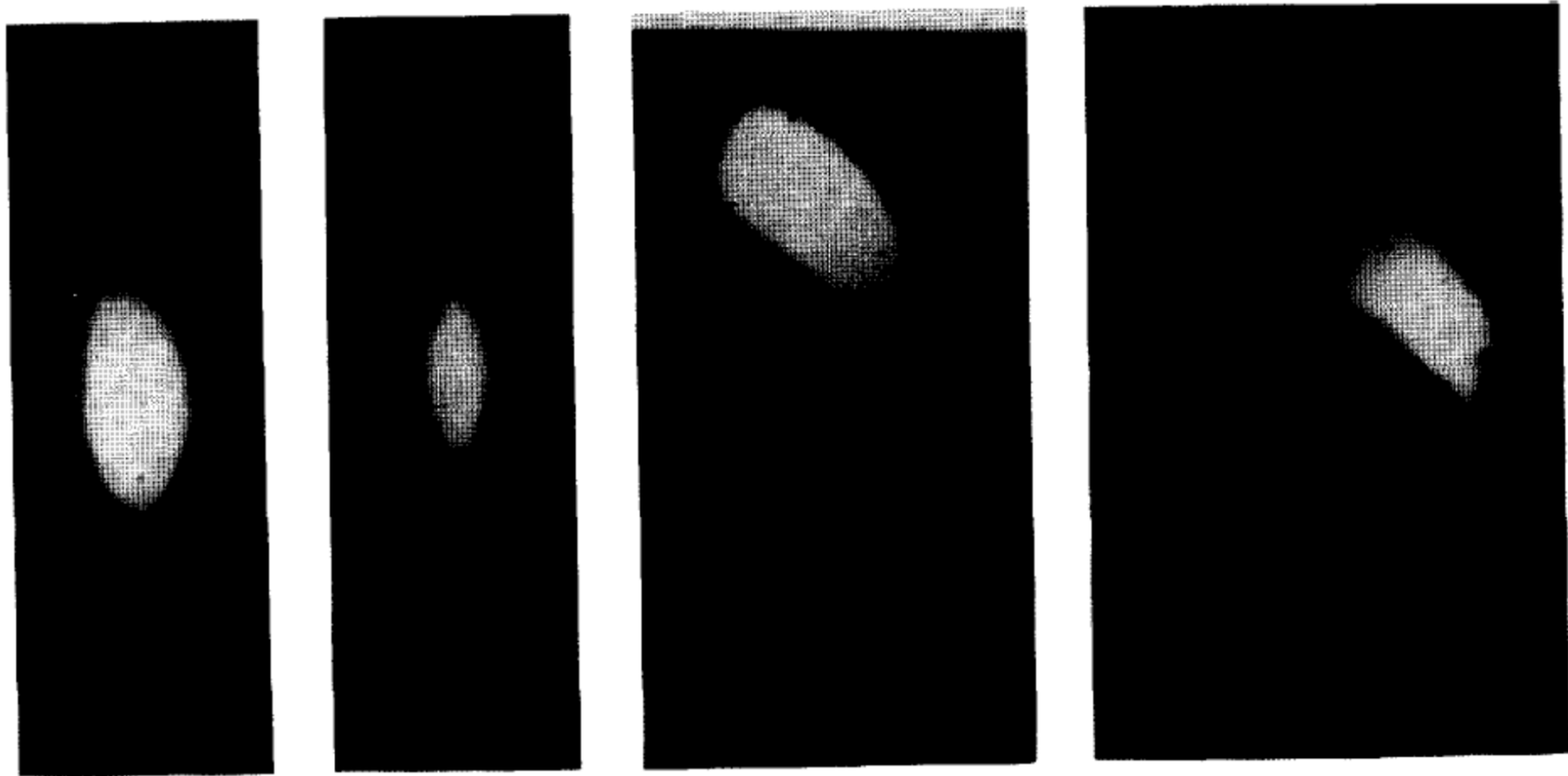


Figure 3.4. Four transverse beam profiles observed at the end of the SLAC linac are shown when the beam was carefully injected and injected with 0.2, 0.5, and 1 mm offsets. The beam sizes σ_x and σ_y are about $120 \mu\text{m}$. (Courtesy John Seeman, 1991.)

Many pictures and derivations used in the slides are taken from the following references:

- [1] 'Wake and Impedance' by G.V. Stupakov, SLAC-PUB-8683;
- [2] 'Physics of Intensity Dependent Instabilities' by K.Y. Ng, Lecture Notes in USPAS 2002;
- [3] 'Accelerator Physics' by S.Y. Lee;
- [4] 'Physics of Collective Beam Instabilities in High Energy Accelerators' by A. Chao;
- [5] 'Impedances and Wakes in High-Energy Particle Accelerators' by B. Zotter and S. Kheifets.

Backup Slides

Homework

- Show that the electric field of an ultra-relativistic charged particle with charge q is given by (Hint: you do not need to derive the delta function, just justify the coefficient.)

$$\vec{E} = \frac{q\hat{r}}{2\pi\epsilon_0 r} \delta(z - ct)$$

- Show that the longitudinal and transverse impedances satisfy the following relations:

$$Z_{//}^*(\omega) = Z_{//}(-\omega) \quad Z_{\perp}^*(\omega) = -Z_{\perp}(-\omega)$$

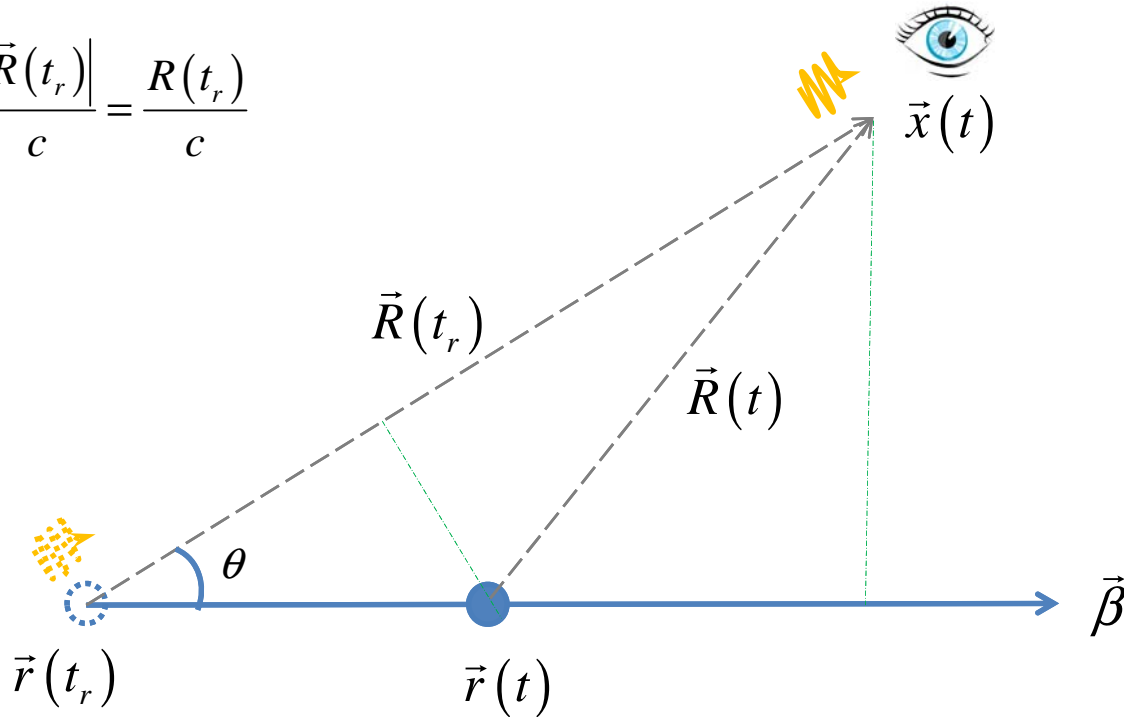
Electric and magnetic field from a charge moving with constant velocity

$$\begin{aligned}\vec{E}(\vec{x}, t) &= \frac{e}{4\pi\epsilon_0\gamma^2(t_r)} \frac{(\vec{n}(t_r) - \vec{\beta}(t_r))}{R(t_r)^2 [1 - \vec{n}(t_r) \cdot \vec{\beta}(t_r)]^3} + \frac{e}{4\pi\epsilon_0 c} \frac{\vec{n} \times [(\vec{n}(t_r) - \vec{\beta}(t_r)) \times \dot{\vec{\beta}}(t_r)]}{R(t_r) [1 - \vec{n}(t_r) \cdot \vec{\beta}(t_r)]^3} \\ &= \vec{E}_{static}(\vec{x}, t) + \vec{E}_{rad}(\vec{x}, t)\end{aligned}$$

$$\vec{E}_{static}(\vec{x}, t) = \frac{e}{4\pi\epsilon_0\gamma^2} \frac{(\vec{n}(t_r) - \vec{\beta}(t_r))}{R(t_r)^2 [1 - \vec{n}(t_r) \cdot \vec{\beta}(t_r)]^3}$$

Rewriting Static Field I:

$$\Delta t = t - t_r = \frac{|\vec{R}(t_r)|}{c} = \frac{R(t_r)}{c}$$



$$\vec{r}(t) - \vec{r}(t_r) = \vec{\beta}c \frac{R(t_r)}{c} = \vec{R}(t_r) - \vec{R}(t) \Rightarrow \vec{R}(t) = \vec{R}(t_r) - \vec{\beta}R(t_r) \Rightarrow \frac{\vec{R}(t)}{R(t_r)} = \vec{n}(t_r) - \vec{\beta}$$

$$\frac{\vec{n}(t_r) \cdot \vec{R}(t)}{R(t_r)} = 1 - \vec{n}(t_r) \cdot \vec{\beta}$$

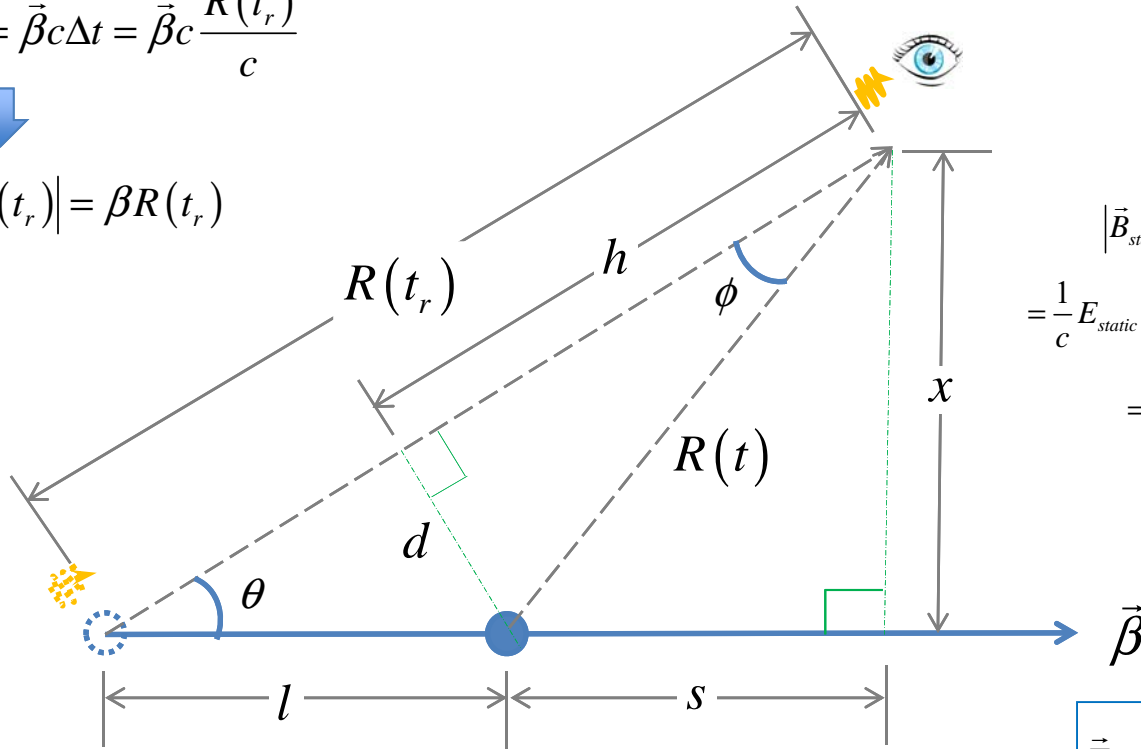
$$\vec{E}_{static}(\vec{x}, t) = \frac{e}{4\pi\epsilon_0\gamma^2} \frac{(\vec{n}(t_r) - \vec{\beta}(t_r))}{R(t_r)^2 [1 - \vec{n}(t_r) \cdot \vec{\beta}(t_r)]^3} = \frac{e}{4\pi\epsilon_0\gamma^2} \frac{\vec{R}(t)}{[\vec{n}(t_r) \cdot \vec{R}(t)]^3}$$

Rewriting Static Field II:

$$\vec{r}(t) - \vec{r}(t_r) = \vec{\beta} c \Delta t = \vec{\beta} c \frac{R(t_r)}{c}$$



$$l = |\vec{r}(t) - \vec{r}(t_r)| = \beta R(t_r)$$



$$\begin{aligned} |\vec{B}_{static}| &= \frac{1}{c} |\vec{n} \times \vec{E}_{static}| = \frac{1}{c} E_{static} \sin \phi \\ &= \frac{1}{c} E_{static} \frac{d}{R(t)} = \frac{1}{c} E_{static} \frac{\beta x}{R(t)} = \frac{1}{c} \beta E_{static} \frac{x}{R(t)} \\ &= \frac{1}{c} \beta E_{static} \sin \psi = \frac{1}{c} |\vec{\beta} \times \vec{E}_{static}| \end{aligned}$$

$$\sin \theta = \frac{x}{R(t_r)}$$



$$d^2 = l^2 \sin^2 \theta = \beta^2 R(t_r)^2 \frac{x^2}{R(t_r)^2} = \beta^2 x^2$$



$$h^2 = R(t)^2 - d^2 = x^2 + s^2 - \beta^2 x^2 = x^2 \gamma^{-2} + s^2 \longrightarrow \vec{n}(t_r) \cdot \vec{R}(t) = \sqrt{s^2 + x^2 \gamma^{-2}}$$

$$\vec{n}(t_r) \cdot \vec{R}(t) = \frac{\vec{R}(t_r) \cdot \vec{R}(t)}{R(t_r)} = R(t) \cos \phi = h$$



$$\begin{aligned} \vec{E}_{static}(\vec{x}, t) &= \frac{e}{4\pi\epsilon_0\gamma^2} \frac{\vec{R}(t)}{[\vec{n}(t_r) \cdot \vec{R}(t)]^3} \\ &= \frac{e}{4\pi\epsilon_0\gamma^2} \frac{\vec{R}(t)}{(s^2 + x^2\gamma^{-2})^{3/2}} \end{aligned}$$



Longitudinal Microwave Instability

Unperturbed phase space density:

$$\psi_0(z, \Delta E) = \psi_0(\Delta E) = \frac{N}{C_0} f_0(\Delta E) \quad \rho_0(z) = \rho_0 = \frac{N}{C_0}$$

$$C_0 = 2\pi R$$

DC current does not excite wake

$$\begin{aligned} V_{//}(z_0) &= \int_{z_0}^{\infty} \lambda(z_1) w_{//}(z_1 - z_0) dz_1 \\ &= \rho_0 \int_{z_0}^{\infty} W_0'(z_1 - z_0) dz_1 = -\rho_0 W_0(0) = 0 \end{aligned}$$

Consider perturbation in phase space density: n-th azimuthal mode

$$\psi_1(z, \Delta E, 0) = \hat{\psi}_1(\Delta E) e^{inz/R}$$

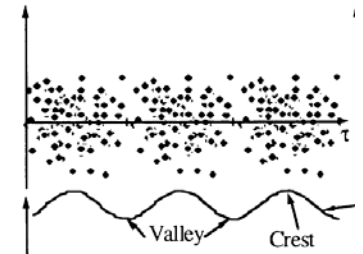
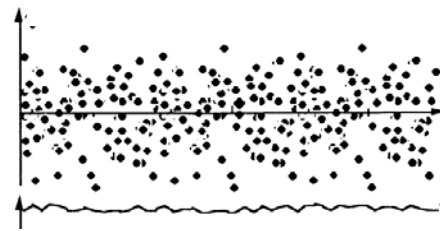
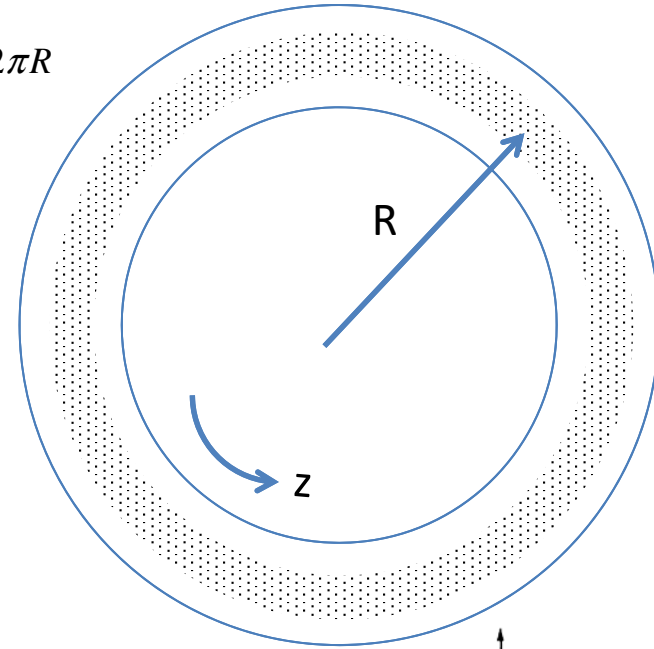
$$\text{Ansatz: } \psi_1(z, \Delta E, t) = \hat{\psi}_1(\Delta E) e^{inz/R - i\Omega t}$$

*Note that if a perturbation is static,

$$\psi_1^*(z, \Delta E, t) = \hat{\psi}_1^*(\Delta E) e^{in(z-v_0t)/R} = \hat{\psi}_1^*(\Delta E) e^{inz/R - i\Omega^* t} \Rightarrow \Omega^* = nv_0 / R = n2\pi v_0 / C = n\omega_0$$

But the system is not likely to be static and we need to solve Vlasov equation self-consistently to know the answer for Ω and hence $\psi_1(s, \Delta E, t)$

$$\frac{\partial}{\partial t} \psi_1(z, \Delta E, t) + \frac{dz}{dt} \cdot \frac{\partial}{\partial z} \psi_1(z, \Delta E, t) + \frac{d\Delta E}{dt} \cdot \frac{\partial}{\partial \Delta E} \psi_0(\Delta E) = 0 \quad \frac{dz}{dt} = v(\Delta E)$$



Longitudinal Microwave Instability

$$c\Delta p_z(z,t) = -eQ_e V_{//}(z,t) = -e^2 v_0 \int_{-\infty}^t \rho_1(z,t_1) w_{//}(t-t_1) dt_1 = -e^2 v_0 \int_0^{\infty} \rho_1(z,t-\tau) w_{//}(\tau) d\tau$$

$\rho_1 v_0 dt$ gives particle number in the slice $(t,t+dt)$.

$T_0 = \frac{C_0}{v_0}$ is revolution period

$$\frac{d\Delta E(z,t)}{dt} = -\frac{c\Delta p_z(z,t)}{T_0} = -\frac{e^2 v_0}{T_0} \int_0^{\infty} \rho_1(z,t-\tau) w_{//}(\tau) d\tau$$

$$w_{//}(\tau) = \frac{1}{2\pi} \int_{-\infty}^{\infty} Z_{//}(\omega) e^{-i\omega\tau} d\omega \quad \rho_1(z,t) = \int_{-\infty}^{\infty} \psi_1(z,\Delta E,t) d\Delta E = \hat{\rho}_1 e^{inz/R-i\Omega t} \quad \hat{\rho}_1 \equiv \int_{-\infty}^{\infty} \hat{\psi}_1(\Delta E) d\Delta E$$

$$\frac{d\Delta E(z,t)}{dt} = -\hat{\rho}_1 \frac{e^2 v_0}{2\pi T_0} e^{inz/R-i\Omega t} \int_{-\infty}^{\infty} d\omega Z_{//}(\omega) \int_{-\infty}^{\infty} e^{i(\Omega-\omega)\tau} d\tau = -\hat{\rho}_1 \frac{e^2 v_0}{T_0} e^{inz/R-i\Omega t} Z_{//}(\Omega)$$

$$-i\Omega \psi_1(z,\Delta E,t) + v(\Delta E) \cdot \frac{in}{R} \psi_1(z,\Delta E,t) - \hat{\rho}_1 \frac{e^2 v_0}{T_0} e^{inz/R-i\Omega t} Z_{//}(\Omega) \cdot \frac{\partial}{\partial \Delta E} \psi_0(\Delta E) = 0$$

$$\psi_1(z,\Delta E,t) = \frac{ie^2 v_0 Z_{//}(\Omega)}{T_0} \frac{\hat{\rho}_1 e^{inz/R-i\Omega t}}{\Omega - \omega(\Delta E)n} \frac{d\psi_0(\Delta E)}{d\Delta E} \quad \omega(\Delta E) = \frac{v(\Delta E)}{R}$$

$$\int_{-\infty}^{\infty} d\Delta E \rightarrow$$

Longitudinal Microwave Instability

Dispersion relation:

$$I_0 = eN/T_0$$

$$1 = \frac{ieI_0 Z_{//}(\Omega)}{T_0} \int_{-\infty}^{\infty} \frac{f_0'(\Delta E)}{\Omega - \omega(\Delta E)n} d\Delta E$$

$$\psi_0(\Delta E) = \frac{N}{C_0} f_0(\Delta E)$$

$$\omega(\Delta E) = \omega_0 + \Delta\omega(\Delta E) = \omega_0 - \eta\omega_0 \frac{\Delta p_z}{p_{0,z}} = \omega_0 - \frac{\eta\omega_0}{\beta^2} \frac{\Delta E}{E_0}$$

*Phase slip factor: $\eta = \frac{1}{\gamma_t^2} - \frac{1}{\gamma^2}$

Cold Beam: $f_0(\Delta E) = \delta(\Delta E)$

*Imaginary part of Ω tell us whether the system is stable

$$1 = \frac{ieI_0 Z_{//}(\Omega)}{T_0} \frac{\eta n \omega_0}{E_0 \beta^2} \int_{-\infty}^{\infty} \frac{f_0(\Delta E)}{\left(\Omega - n\omega_0 + \frac{\eta n \omega_0}{E_0 \beta^2} \Delta E \right)^2} d\Delta E$$

$$\psi_1(z, \Delta E, t) = \hat{\psi}_1(\Delta E) e^{inz/R - i\Omega t}$$

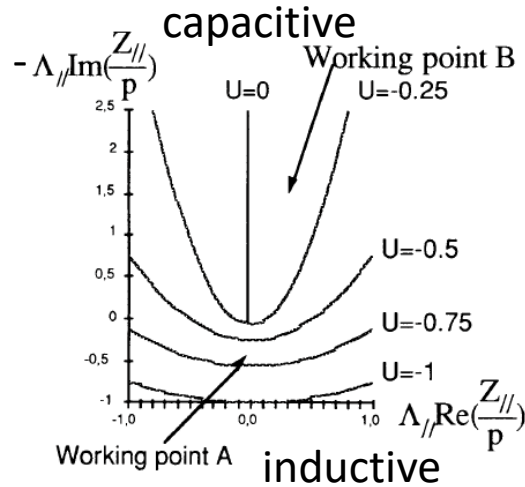
$$\Rightarrow \Omega = n\omega_0 \pm \omega_0 \sqrt{\frac{ieI_0 \eta n Z_{//}(\Omega)}{2\pi E_0 \beta^2}} \approx n\omega_0 \pm \omega_0 \sqrt{\frac{ieI_0 \eta n Z_{//}(n\omega_0)}{2\pi E_0 \beta^2}}$$

Perturbative approach assuming $\frac{|\Omega - n\omega_0|}{n\omega_0} \ll 1$

Longitudinal Microwave Instabilities

Cold beam continued:

(assuming $\eta > 0$) $\Omega \approx n\omega_0 \pm \omega_0 \sqrt{\frac{ieI_0 \eta n Z_{//}(n\omega_0)}{2\pi E_0 \beta^2}}$



Taken from 'Accelerator Physics' by S.Y. Lee

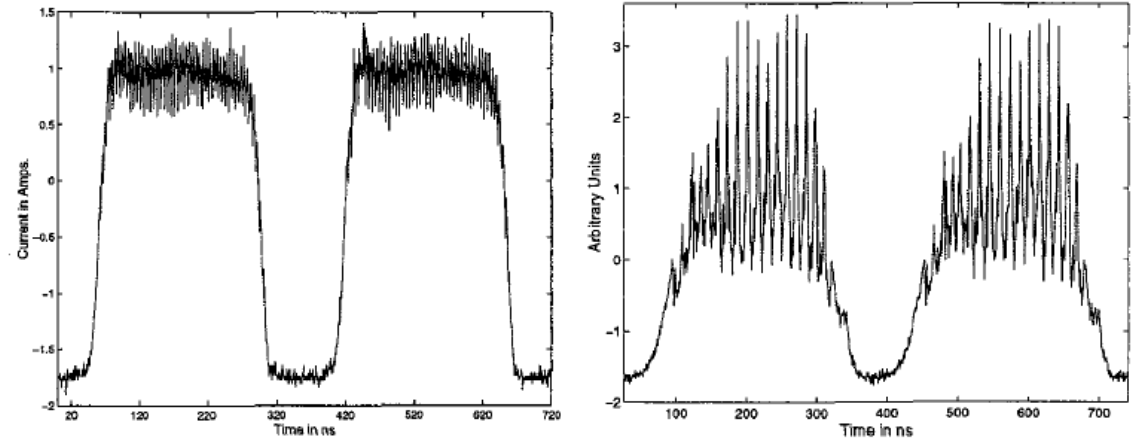


Figure 3.36: The longitudinal beam profiles observed at PSR the bunched coasting beam in the presence of inductive inserts, where three 1-m long ferrite ring cavities were installed in the PSR ring. [Courtesy of R. Macek, LANL]

Taken from S.Y. Lee

Warm Beam:

$$J_G(\tilde{\Omega}) = \sqrt{\frac{2}{\pi}} \int_{-\infty}^{\infty} \frac{-x \exp\left(-\frac{x^2}{2}\right)}{\left[\frac{\tilde{\Omega}}{\eta n \omega_0 \sigma_E} + x\right]} dx$$

$$\tilde{\Omega} = \text{Re}(\tilde{\Omega}) + i \text{Im}(\tilde{\Omega}) \equiv \Omega - \omega_0 n$$

$$\begin{aligned} 1 &= \frac{ieI_0 Z_{//}(n\omega_0)}{T_0} \frac{1}{\sqrt{2\pi\sigma_E^2}} \int_{-\infty}^{\infty} \frac{-\frac{\Delta E}{\sigma_E} \exp\left(-\frac{\Delta E^2}{2\sigma_E^2}\right)}{\Omega - \omega(\Delta E)n} d\Delta E \\ &= i \frac{1}{2} \left\{ \frac{eI_0 [Z_{//}(n\omega_0)/n] E_0 \beta^2}{2\pi \eta \sigma_E^2} \right\} J_G(\tilde{\Omega}) \\ &= i \frac{2 \ln(2)}{\pi} \left\{ \frac{eI_0 [Z_{//}(n\omega_0)/n] E_0 \beta^2}{\eta \sigma_{E,FWHM}^2} \right\} J_G(\tilde{\Omega}) \end{aligned}$$

$$f_0(\Delta E) = \frac{1}{\sqrt{2\pi\sigma_E}} \exp\left(-\frac{\Delta E^2}{2\sigma_E^2}\right)$$

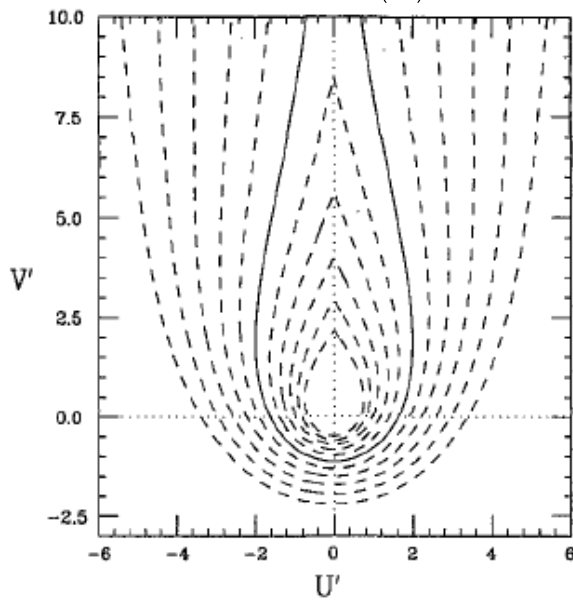
$$U' - iV' \equiv \frac{eI_0 [Z_{//}(n\omega_0)/n] E_0 \beta^2}{\eta \sigma_{E,FWHM}^2}$$

$$U' = \text{Re}(Z_{//}(n\omega_0)) \quad V' = -\text{Im}(Z_{//}(n\omega_0))$$

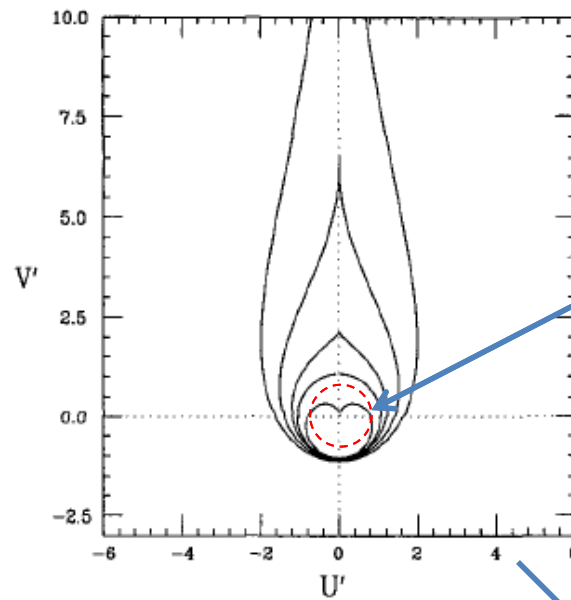
$$U' - iV' = \frac{-i\pi}{2 \ln(2) J_G(\text{Re} \tilde{\Omega} + i \text{Im} \tilde{\Omega})}$$

Longitudinal Microwave instability

Gaussian with various growth rate, $\text{Im}(\tilde{\Omega})$



Contours with $\text{Im}(\tilde{\Omega})=0$ for various energy distribution



Simplified estimation for stability condition:
Keil-Schnell criterion

$$\left| Z_{//}(n\omega_0) / n \right| \leq \frac{2\pi |\eta| \sigma_E^2}{E_0 \beta^2 e I_0} F$$

F depends on distribution and for Gaussian energy distribution, it is 1.

Figure 3.34: Left: The solid line shows the parameters V' vs U' for a Gaussian beam distribution at a zero growth rate. Dashed lines inside the threshold curve are stable. They correspond to $-\text{Im} \Omega / (\sqrt{2 \ln 2} \omega_0 \eta \sigma_\delta) = -0.1, -0.2, -0.3, -0.4,$ and -0.5 . Dashed lines outside the threshold curve have growth rates $-\text{Im} \Omega / (\sqrt{2 \ln 2} \omega_0 \eta \sigma_\delta) = 0.1, 0.2, 0.3, 0.4,$ and 0.5 respectively. Right: The threshold V' vs U' parameters for various beam distributions.

from inside outward, for the normalized distribution functions $\Psi_0(x) = 3(1-x^2)/4,$ $8(1-x^2)^{3/2}/3\pi,$ $15(1-x^2)^2/16,$ $315(1-x^2)^4/32,$ and $(1/\sqrt{2\pi}) \exp(-x^2/2)$. All dis-

Typical Longitudinal Impedance

$$j = -i$$

Taken from 'Coasting beam longitudinal coherent instabilities' by J.L. Laclare

